

Block Diagrams, Signal Flow Graphs, Sensitivity

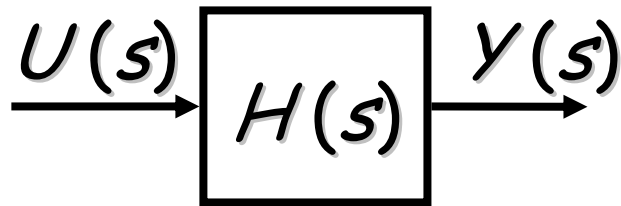
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- Block diagrams
 - rules
- Signal flow graphs
 - Mason's rule
- Sensitivity
 - sensitivity
 - complementary sensitivity
 - steady state errors
 - system type (versus system order)



$$Y(s) = H(s)U(s)$$

$$Y = HU$$

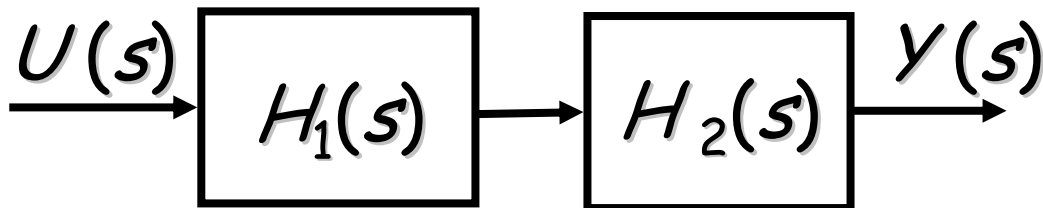
- Linear systems
- Signals:
 - Laplace transformations
- Contents of blocks:
 - transfer functions

lower case

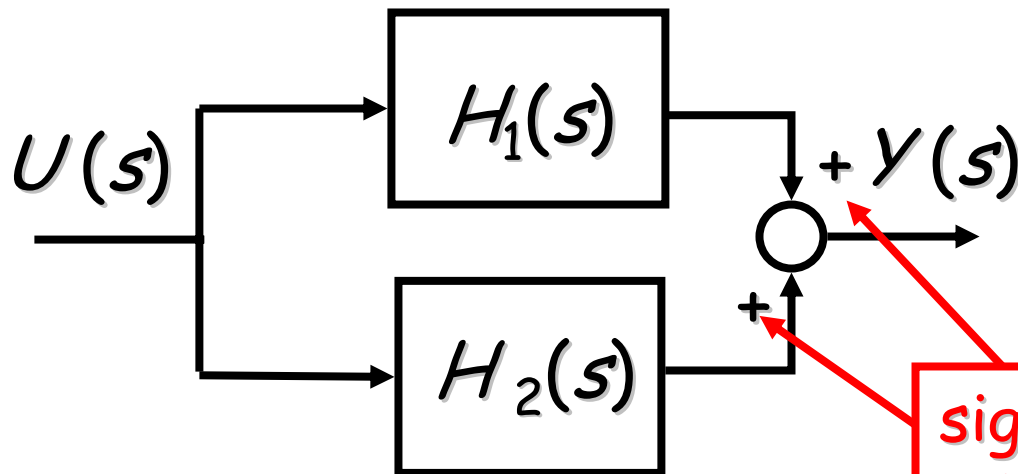
$y(t)$ versus $Y(s)$

capital font

Block diagrams (connections)



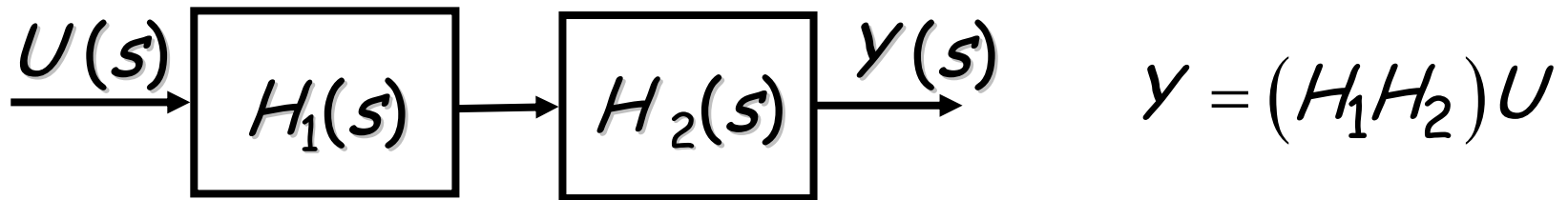
$$Y = H_1 H_2 U$$



$$Y = H_1 U + H_2 U$$
$$= (H_1 + H_2) U$$

signs always
at the left
of arrows

Example (series)



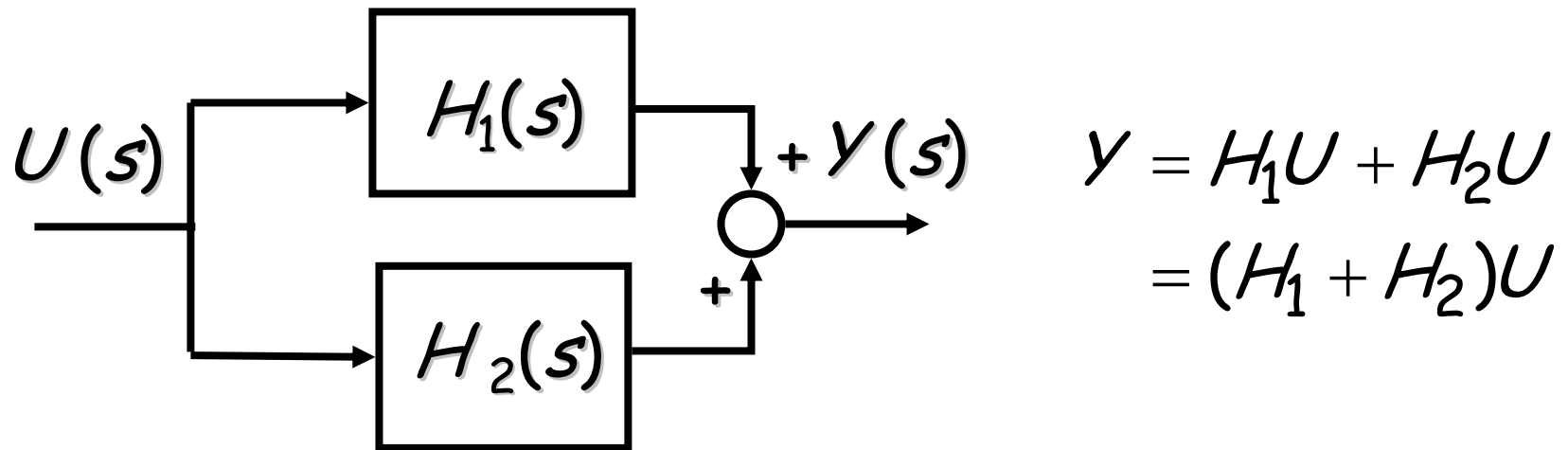
$$H_1 = \frac{K_1}{s\tau_1 + 1}$$

$$H_1 H_2 = \frac{K_1}{s\tau_1 + 1} \frac{K_2}{s\tau_2 + 1}$$

$$H_2 = \frac{K_2}{s\tau_2 + 1}$$

$$= \frac{K_1 K_2}{(s\tau_1 + 1)(s\tau_2 + 1)}$$

Example (parallel)



$$H_1 = \frac{K_1}{s\tau_1 + 1}$$

$$H_1 + H_2 = \frac{K_1}{s\tau_1 + 1} + \frac{K_2}{s\tau_2 + 1}$$

$$H_2 = \frac{K_2}{s\tau_2 + 1}$$

$$= \frac{K_1(s\tau_2 + 1) + K_2(s\tau_1 + 1)}{(s\tau_1 + 1)(s\tau_2 + 1)}$$

Example (parallel)

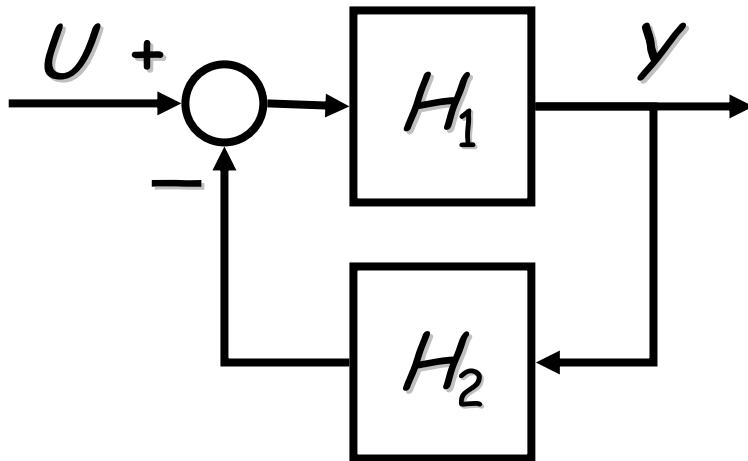
$$\begin{aligned} H_1 + H_2 &= \frac{K_1(s\tau_2 + 1) + K_2(s\tau_1 + 1)}{(s\tau_1 + 1)(s\tau_2 + 1)} \\ &= \frac{(sK_1\tau_2 + K_1) + (sK_2\tau_1 + K_2)}{(s\tau_1 + 1)(s\tau_2 + 1)} = \frac{s(K_1\tau_2 + K_2\tau_1) + K_1 + K_2}{(s\tau_1 + 1)(s\tau_2 + 1)} \end{aligned}$$

$$= (K_1 + K_2) \frac{s \left(\frac{K_1\tau_2 + K_2\tau_1}{K_1 + K_2} \right) + 1}{(s\tau_1 + 1)(s\tau_2 + 1)}$$



zero

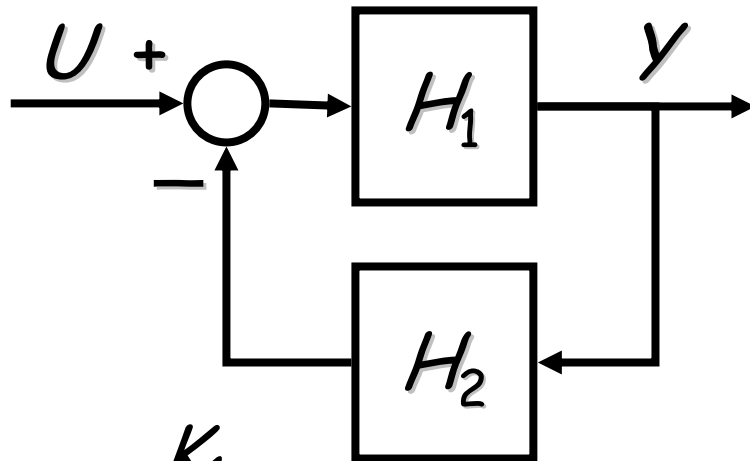
Block diagrams (feedback)



$$y = \frac{H_1}{1 + H_1 H_2} U$$

$$y = \frac{\text{forward path}}{1 - \text{loop transfer}} U$$

Example (feedback)



$$H_1 = \frac{K_1}{s\tau_1 + 1}$$

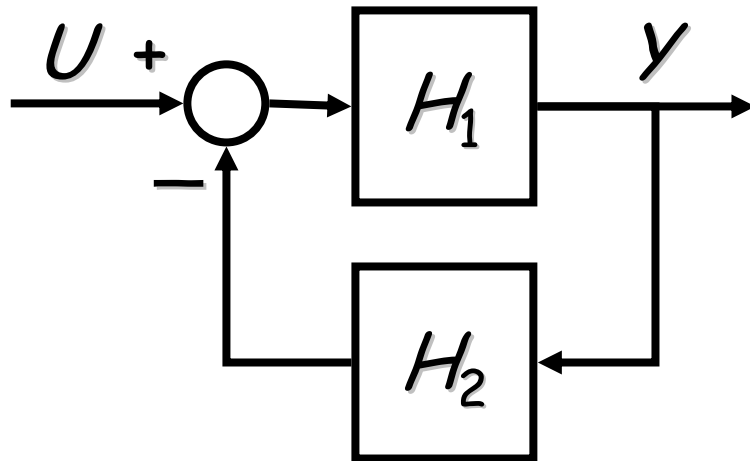
$$H_2 = \frac{K_2}{s\tau_2 + 1}$$

$$Y = HU$$

$$H = \frac{\frac{K_1}{s\tau_1 + 1}}{1 + \frac{K_1}{s\tau_1 + 1} \frac{K_2}{s\tau_2 + 1}}$$

$$= \frac{K_1 (s\tau_2 + 1)}{(s\tau_1 + 1)(s\tau_2 + 1) + K_1 K_2}$$

Example (feedback)

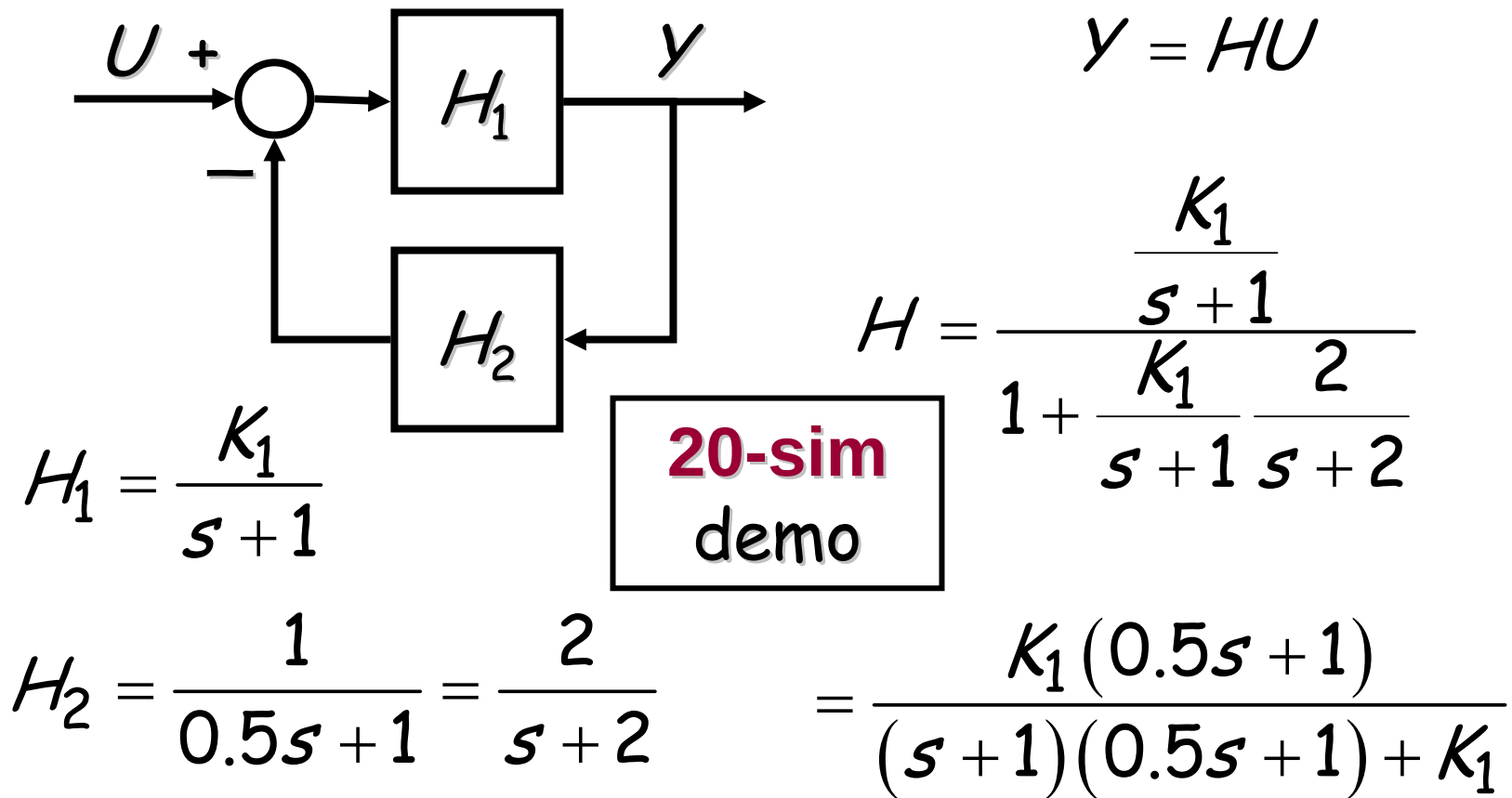


pole of H_2 is
zero of H

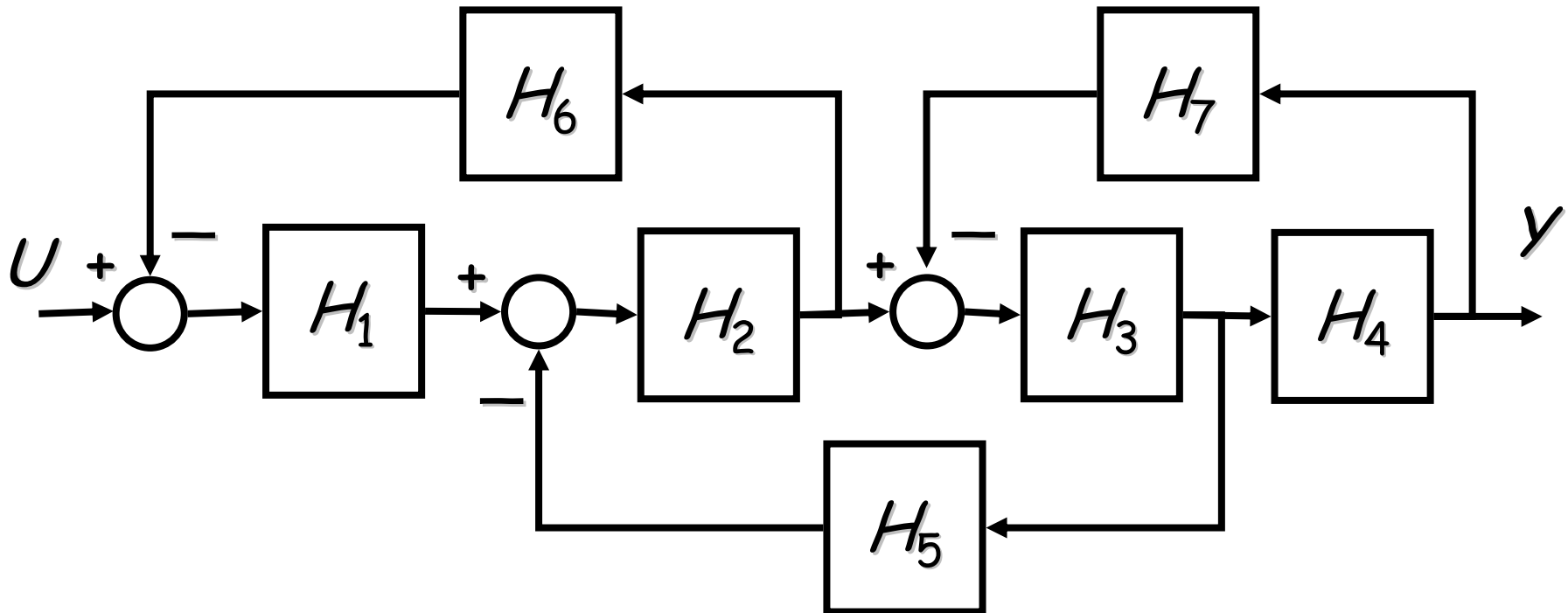
$$H = \frac{K_1(s\tau_2 + 1)}{(s\tau_1 + 1)(s\tau_2 + 1) + K_1K_2}$$

poles of H not equal
to poles of H_1 and H_2

unless $K_1 = 0$
and/or $K_2 = 0$

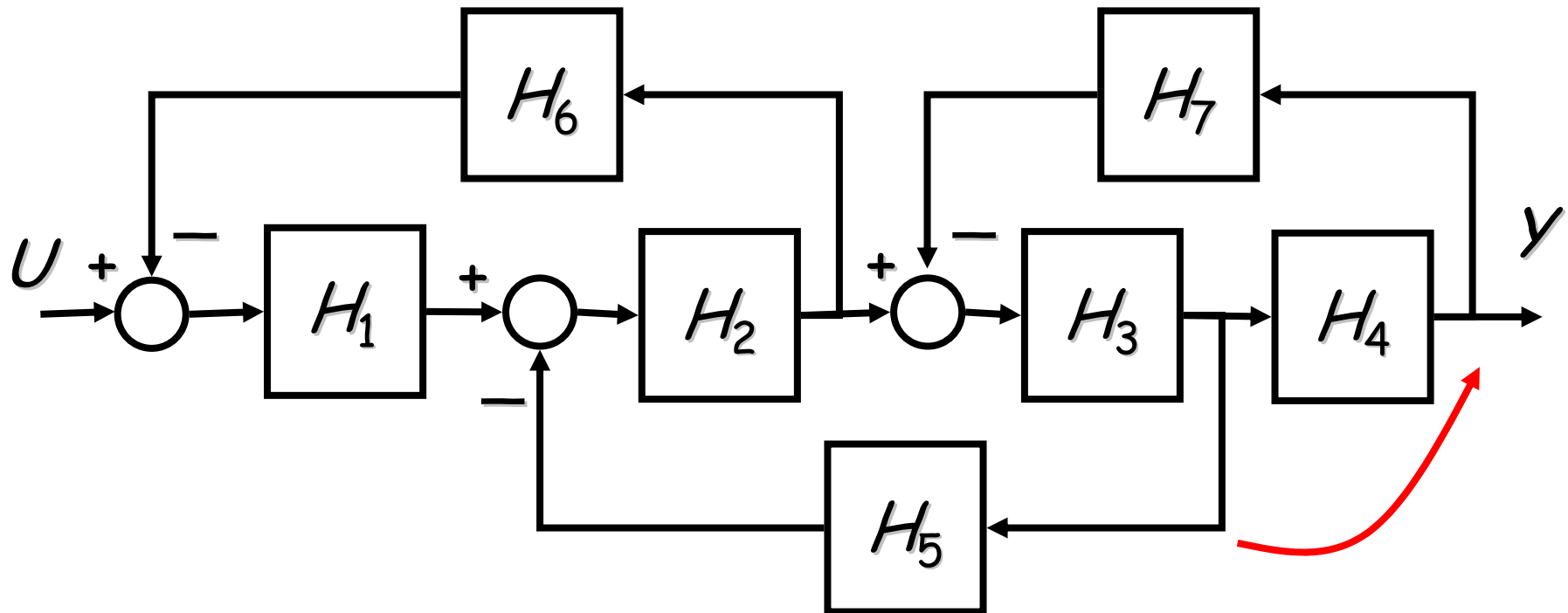


Example (complex system)

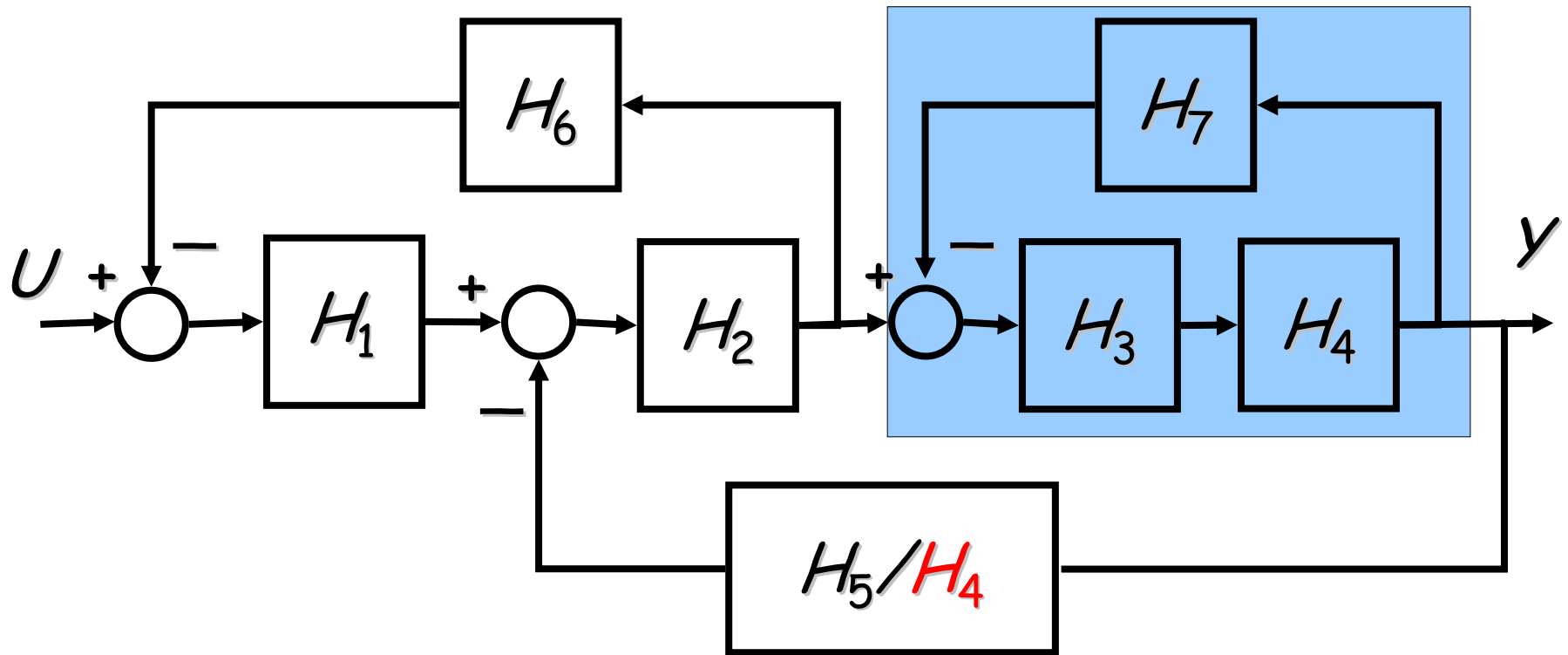


Exercise: Do it yourself

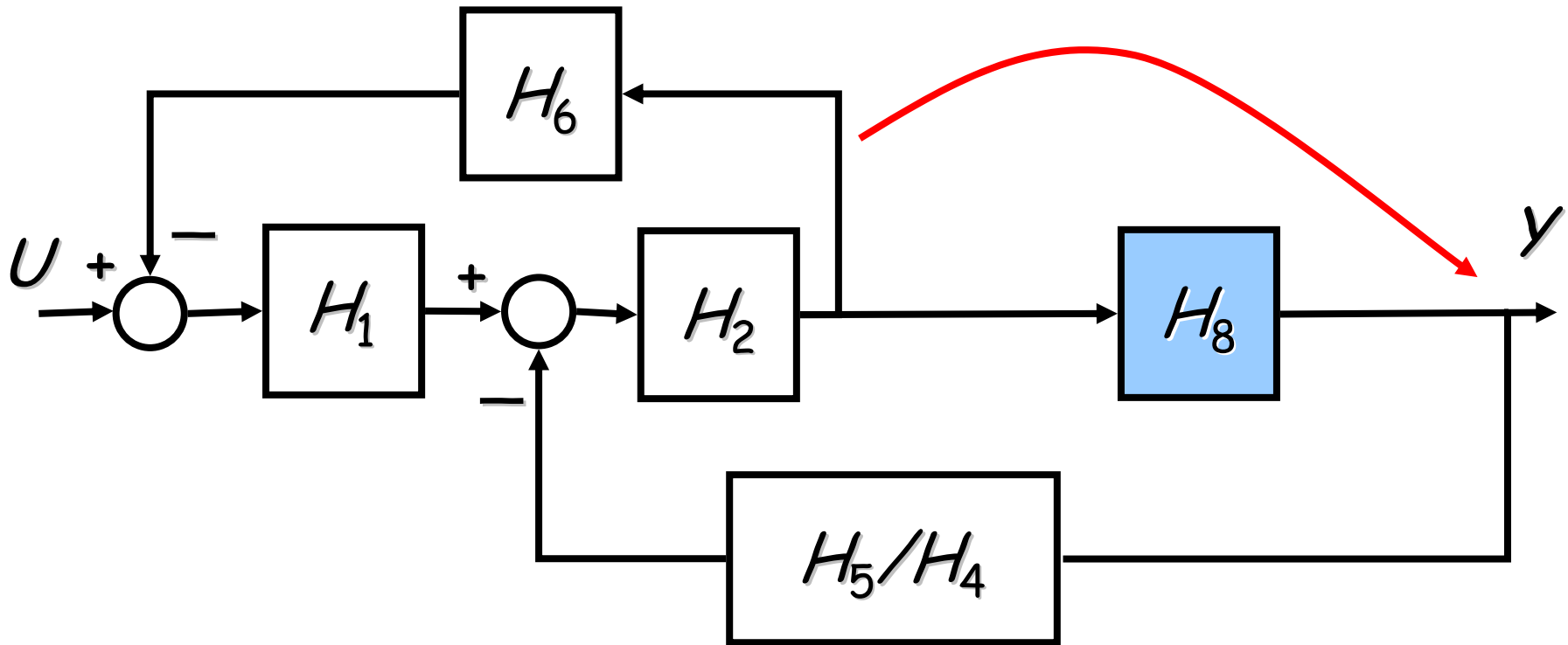
Example (complex system)



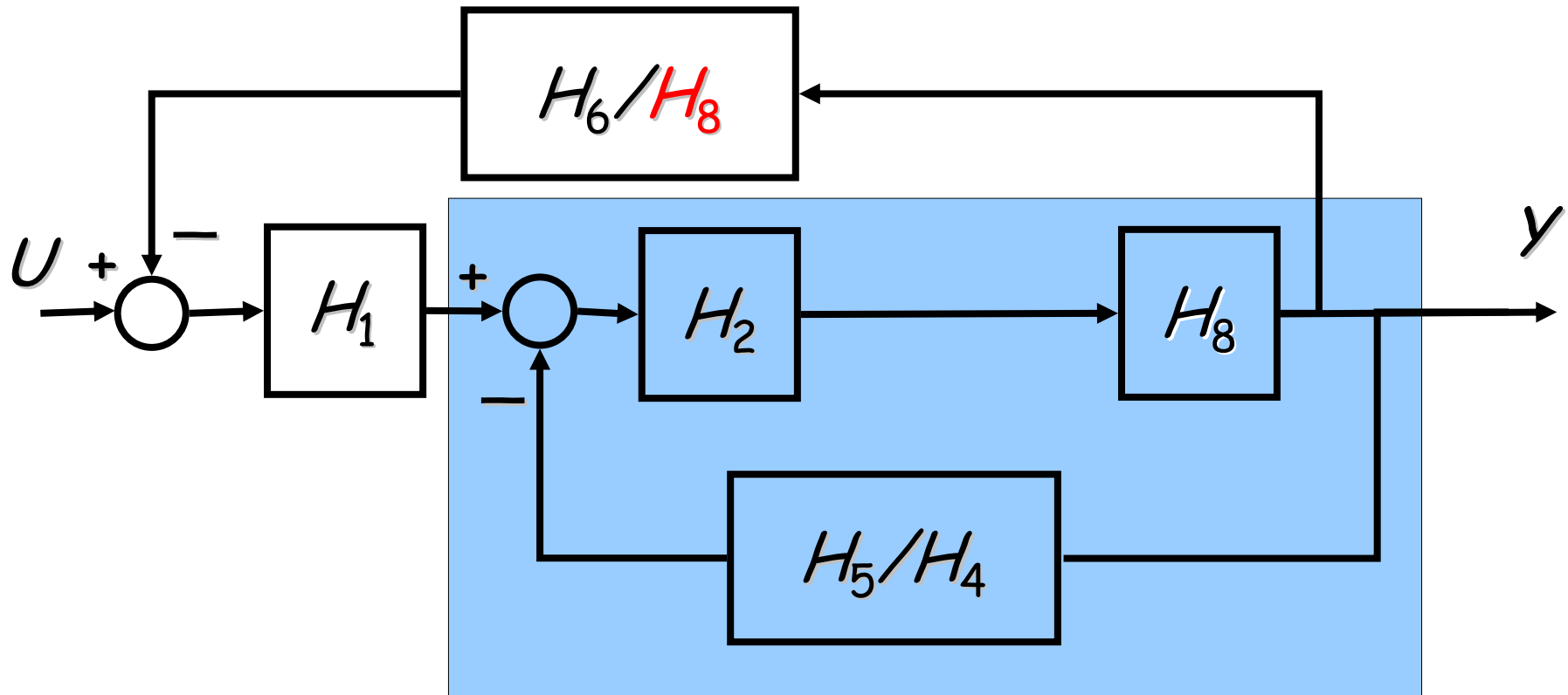
Example (complex system)



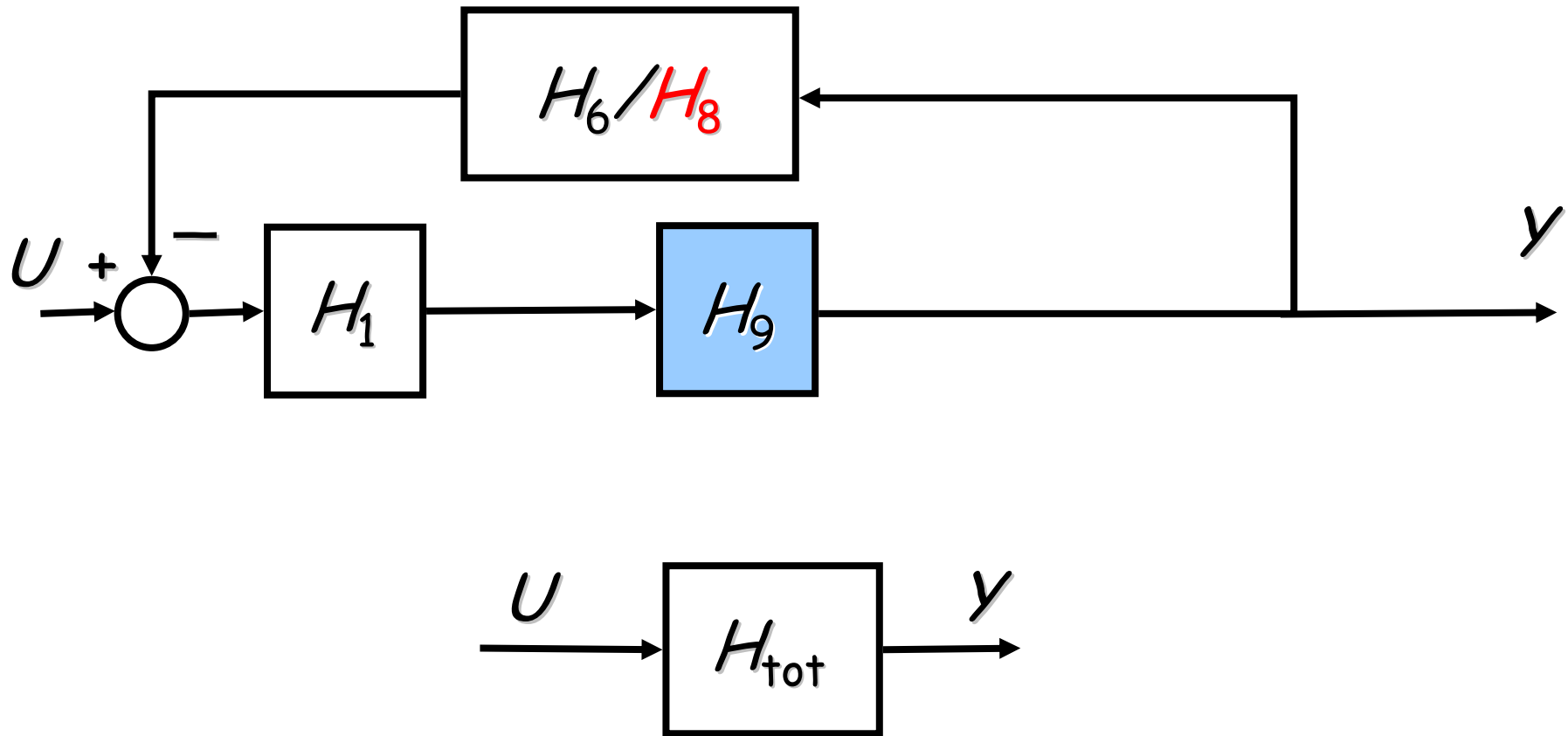
Example (complex system)



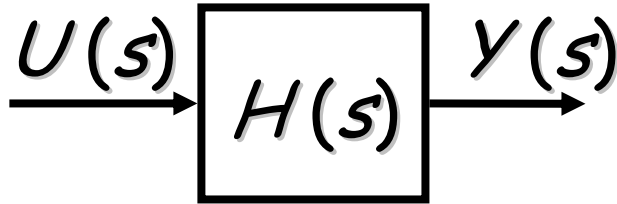
Example (complex system)



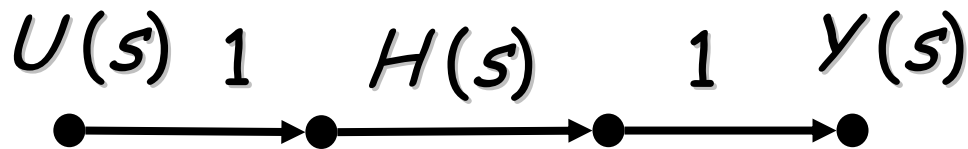
Example (complex system)



- To compute transfer functions of complex diagrams
- Mostly uses signal flow graphs
- With care it can be used with block diagrams as well



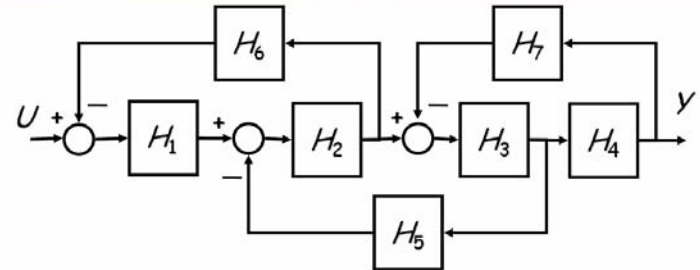
$$Y(s) = H(s)U(s)$$
$$Y = HU$$



- Linear systems
- Nodes:
 - signals
- Branches:
 - transfer functions

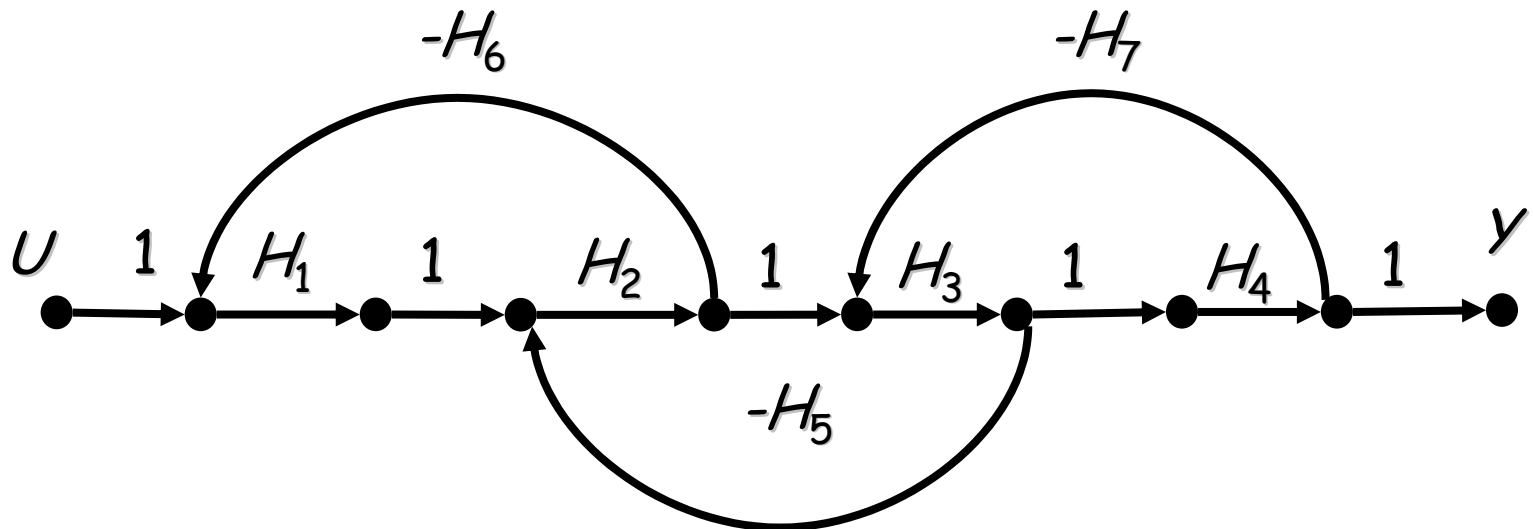
Example

Example (complex system)



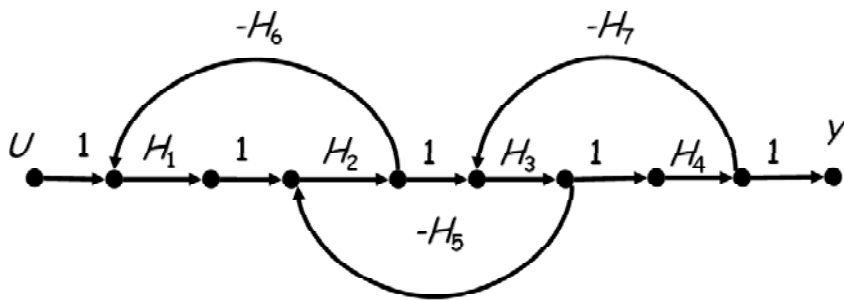
Exercise: Do it yourself

Control Engineering -3- Block diagrams / Sensitivity © Job van Amerongen (12)



- **Path:**

- a succession of branches in the direction of the arrows that do not pass any node more than once

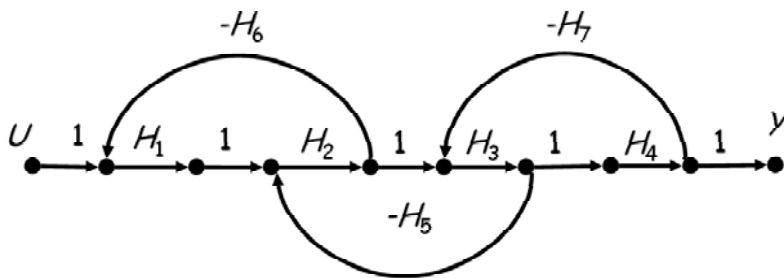


There is 1 path from U to Y

$$H_1 H_2 H_3 H_4 = \text{path gain}$$

- **Loop:**

- a **closed** succession of branches in the direction of the arrows that do not pass any node more than once



There are three loops

$$-H_1 H_2 H_6 = \text{loop gain}$$

$$-H_3 H_4 H_7 = \text{loop gain}$$

$$-H_2 H_3 H_5 = \text{loop gain}$$

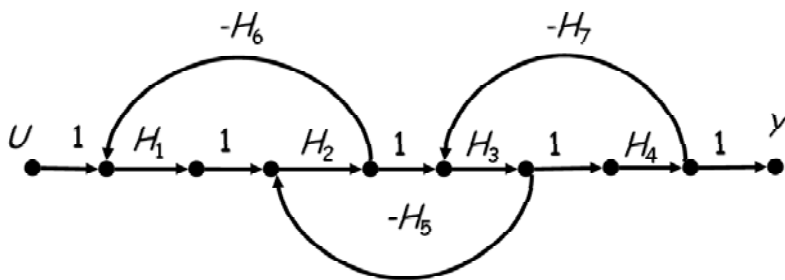
- **Touching:**
- Loops with one or more nodes in common are called **touching**. A loop and a path are touching when they have a common node.

Touching loops:

$-H_1 H_2 H_6$ with $-H_2 H_3 H_5$
 $-H_3 H_4 H_7$ with $-H_2 H_3 H_5$

Non-touching loops:

$-H_1 H_2 H_6$ and $-H_3 H_4 H_7$



- **Determinant:**

- The determinant Δ of a signal flow graph is:

$$\Delta = 1 - (\text{sum of all loop gains})$$

- + (sum of products of gains of all possible combinations of 2 non-touching loops)
- (sum of products of gains of all possible combinations of 3 non-touching loops)
- + ...

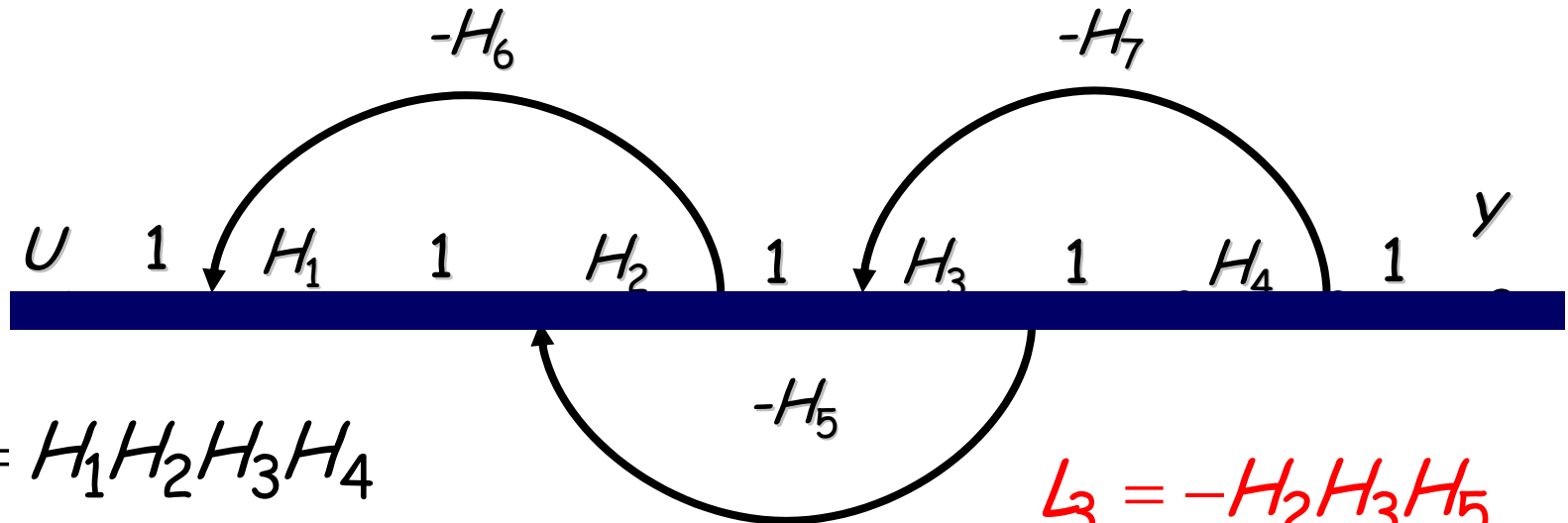
- **Cofactor:**
 - The cofactor of the i -th path, denoted by Δ_i , is the determinant of the signal flow graph formed by deleting all loops touching path i .

$$H(s) = \frac{P_1\Delta_1 + P_2\Delta_2 + \dots}{\Delta}$$

Example

$$L_1 = -H_1H_2H_6$$

$$L_2 = -H_3H_4H_7$$



$$P_1 = H_1H_2H_3H_4$$

$$\Delta_1 = 1$$

(cofactor = 1)

$$\Delta = 1 + H_1H_2H_6 + H_3H_4H_7 + H_2H_3H_5 + H_1H_2H_6H_3H_4H_7$$

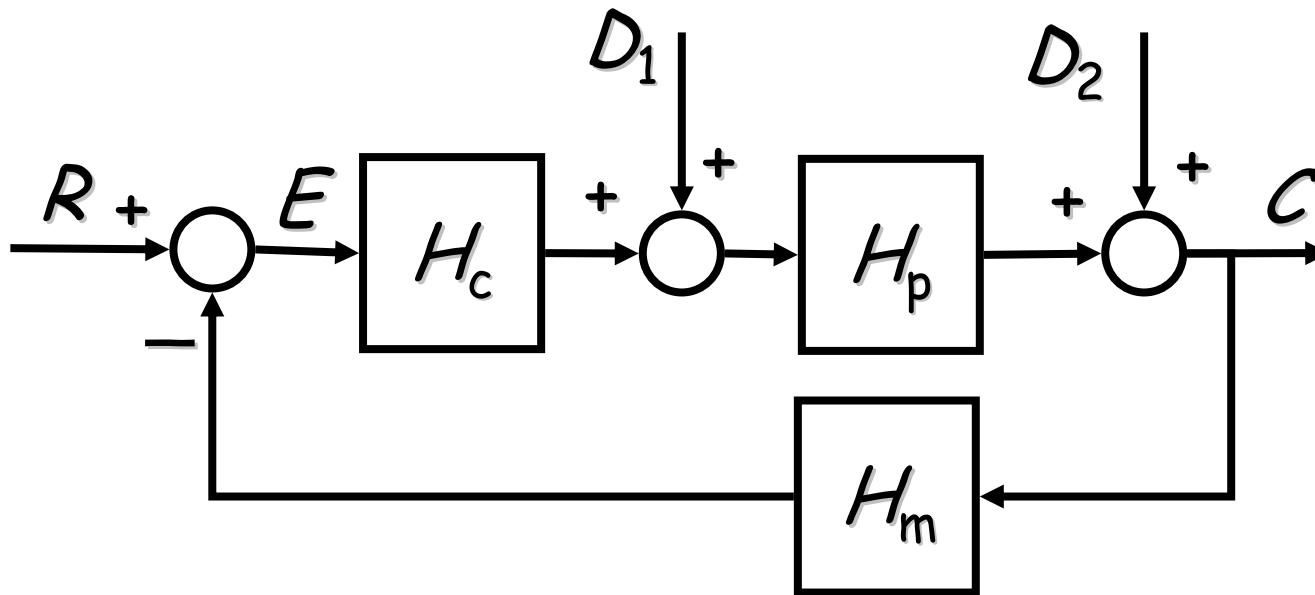
Example

$$P_1 = H_1 H_2 H_3 H_4$$

$$\Delta_1 = 1$$

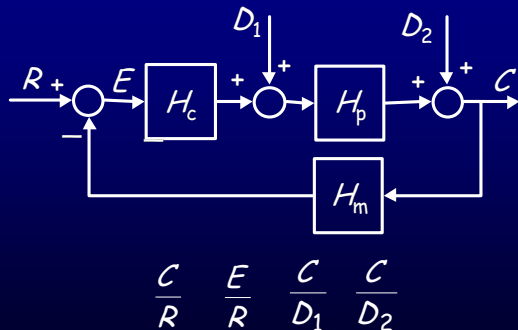
$$\Delta = 1 + H_1 H_2 H_6 + H_3 H_4 H_7 + H_2 H_3 H_5 + H_1 H_2 H_6 H_3 H_4 H_7$$

$$H = \frac{H_1 H_2 H_3 H_4}{1 + H_1 H_2 H_6 + H_3 H_4 H_7 + H_2 H_3 H_5 + H_1 H_2 H_6 H_3 H_4 H_7}$$



$$\frac{C}{R} \quad \frac{E}{R} \quad \frac{C}{D_1} \quad \frac{C}{D_2}$$

Feedback systems



It is important that H_m is constant and in this configuration H_m should be 1

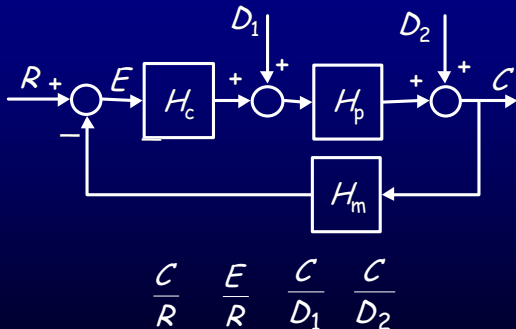
$$\frac{C}{R} = \frac{H_c H_p}{1 + H_c H_p H_m}$$

Desired: $\frac{C}{R} = 1$

$$\longrightarrow \textcircled{H_c H_p} \rightarrow \infty$$

$$\frac{C}{R} \approx \frac{H_c H_p}{H_c H_p H_m} = \frac{1}{H_m}$$

Feedback systems



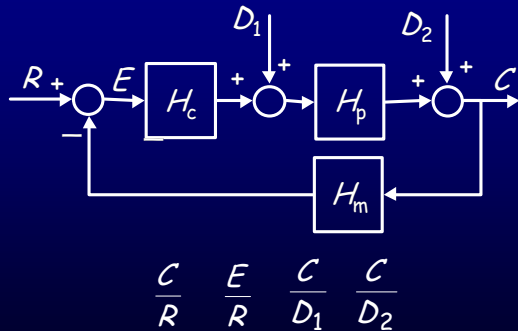
$$\frac{E}{R} = \frac{1}{1 + H_c H_p H_m} = \frac{1}{1 + H_L}$$

Desired: $\frac{E}{R} = 0$

$$\longrightarrow H_L = H_c H_p H_m \rightarrow \infty$$

$$\frac{E}{R} \approx \frac{1}{\infty} \rightarrow 0$$

Feedback systems



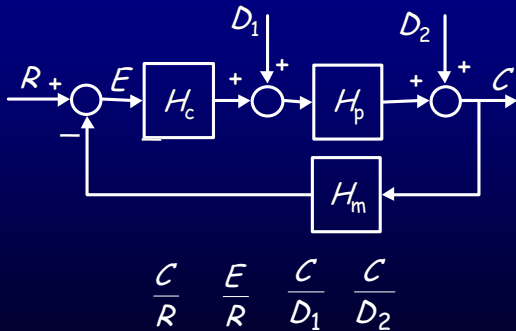
$$\frac{C}{D_1} = \frac{H_p}{1 + H_c H_p H_m}$$

Desired: $\frac{C}{D_1} = 0$

$$\longrightarrow H_c H_m \rightarrow \infty$$

$$\frac{C}{D_1} \approx \frac{H_p}{H_c H_p H_m} = \frac{1}{H_c H_m} \rightarrow 0$$

Feedback systems



$$\frac{C}{D_2} = \frac{1}{1 + H_c H_p H_m} = \frac{1}{1 + H_L}$$

Desired: $\frac{C}{D_2} = 0$

$$\longrightarrow H_c H_m H_p \rightarrow \infty$$

$$\frac{C}{D_2} \approx \frac{1}{H_c H_p H_m} \rightarrow 0$$

Conclusion

$$\begin{aligned}\frac{C}{R} = 1 &\longrightarrow H_c H_p \rightarrow \infty \\ \frac{E}{R} = 0 &\longrightarrow H_c H_p H_m \rightarrow \infty \\ \frac{C}{D_1} = 0 &\longrightarrow H_c H_m \rightarrow \infty \\ \frac{C}{D_2} = 0 &\longrightarrow H_c H_p H_m \rightarrow \infty\end{aligned}$$

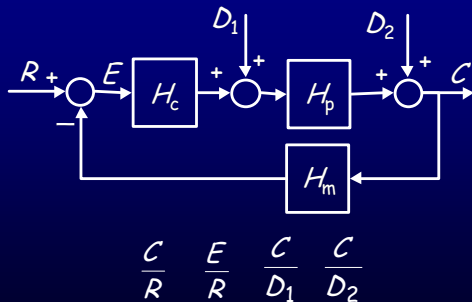
All goals can be
achieved when

$$H_c \rightarrow \infty$$



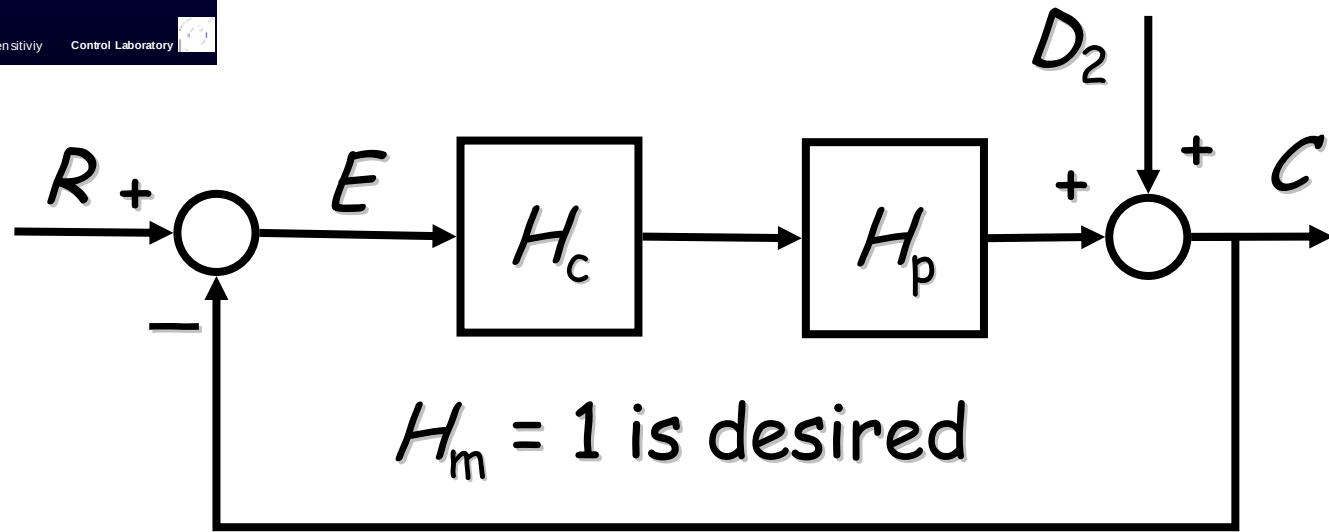
$$H_{\text{sensor}} = 1$$

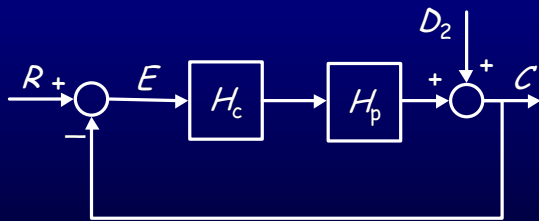
Feedback systems



if $H_c H_p \rightarrow \infty$

$$\frac{C}{R} \approx \frac{H_c H_p}{H_c H_p H_m} = \frac{1}{H_m}$$





$$\frac{C}{D_2} = \frac{1}{1 + H_c H_p}$$

$$\frac{C}{R} = \frac{H_c H_p}{1 + H_c H_p}$$

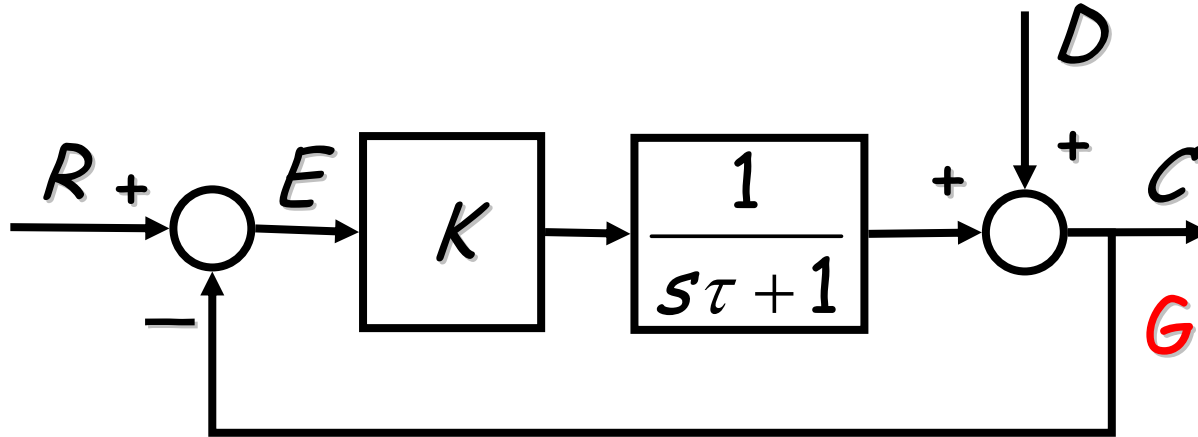
$$\frac{1}{1 + H_c H_p}$$

Sensitivity

$$+ \frac{H_c H_p}{1 + H_c H_p} = 1$$

Complementary Sensitivity

Example (type 0)



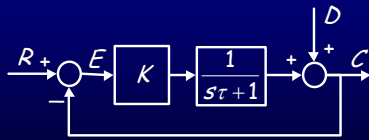
$G(s)$ = first order

$$\frac{C}{D} = \frac{1}{1 + \frac{K}{s\tau + 1}} = \frac{1}{1 + KG(s)}$$

pure integrators = 0
(type 0)

$$\frac{C}{D} = \frac{s\tau + 1}{s\tau + 1 + K} = \left(\frac{1}{1 + K} \right) \left(\frac{s\tau + 1}{s \frac{\tau}{1 + K} + 1} \right)$$

Example (type 0)



$$\frac{C}{D} = \left(\frac{1}{1+K} \right) \left(\frac{s\tau + 1}{s \frac{\tau}{1+K} + 1} \right)$$

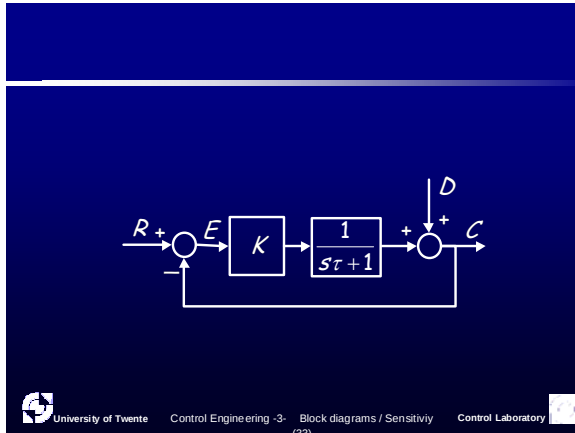
if $D = 1/s$

$$\lim_{t \rightarrow \infty} c(t)$$

$$= \lim_{s \rightarrow 0} \left[\frac{s}{s} \left(\frac{1}{1+K} \right) \left(\frac{s\tau + 1}{s \frac{\tau}{1+K} + 1} \right) \right] = \frac{1}{1+K}$$

ϵ_{ss}

Example (type 0)

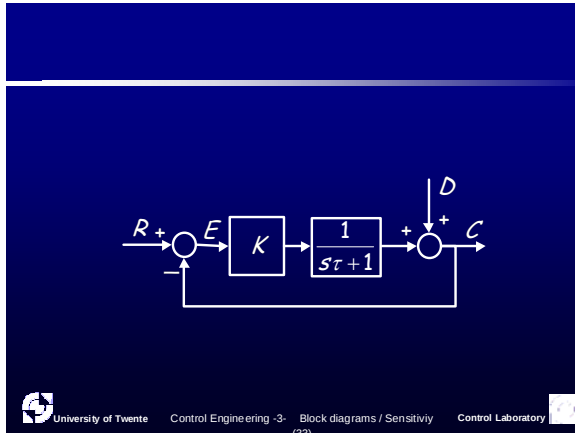


$$\frac{C}{D} = \left(\frac{1}{1+K} \right) \left(\frac{s\tau + 1}{s \frac{\tau}{1+K} + 1} \right)$$

if $D = 1/s$

$$\lim_{t \rightarrow 0} c(t) = \lim_{s \rightarrow \infty} \left[\frac{s}{s} \left(\frac{1}{1+K} \right) \left(\frac{s\tau + 1}{s \frac{\tau}{1+K} + 1} \right) \right] = \frac{1}{1+K} \frac{\tau}{\frac{\tau}{1+K}} = 1$$

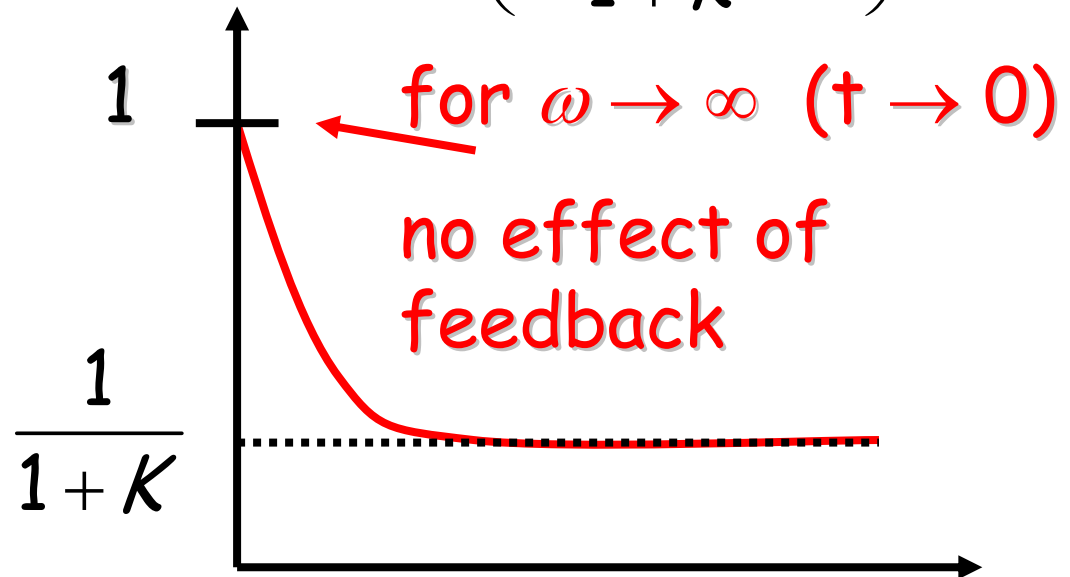
Example (type 0)



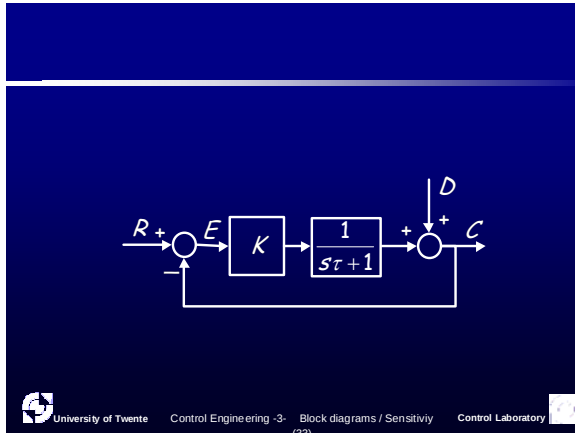
steady state
error:

$$\varepsilon_{ss} = \frac{1}{1 + K}$$

$$\frac{C}{D} = \left(\frac{1}{1 + K} \right) \left(\frac{s\tau + 1}{s \frac{\tau}{1 + K} + 1} \right)$$



Demo 20-sim (type 0)

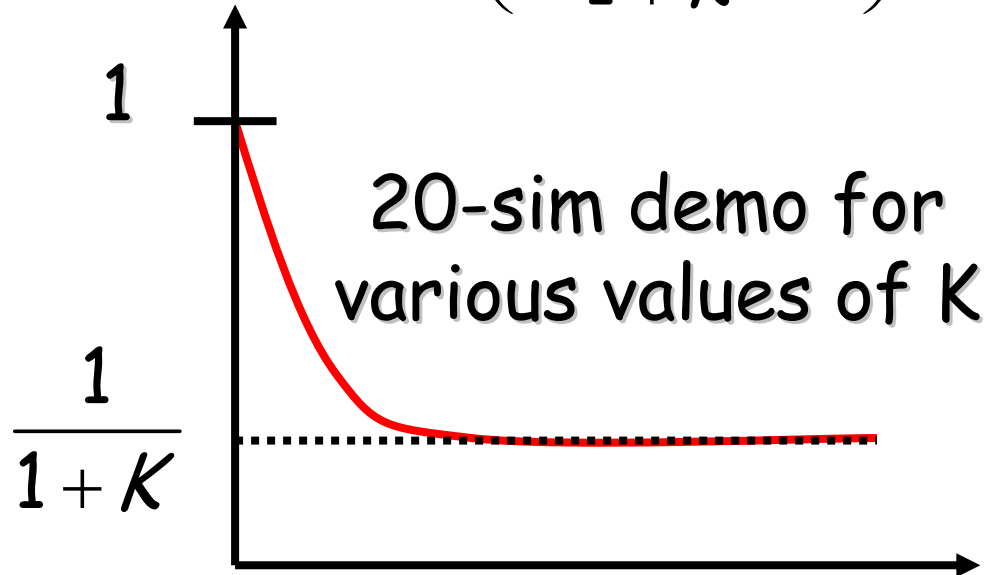


steady state
error:

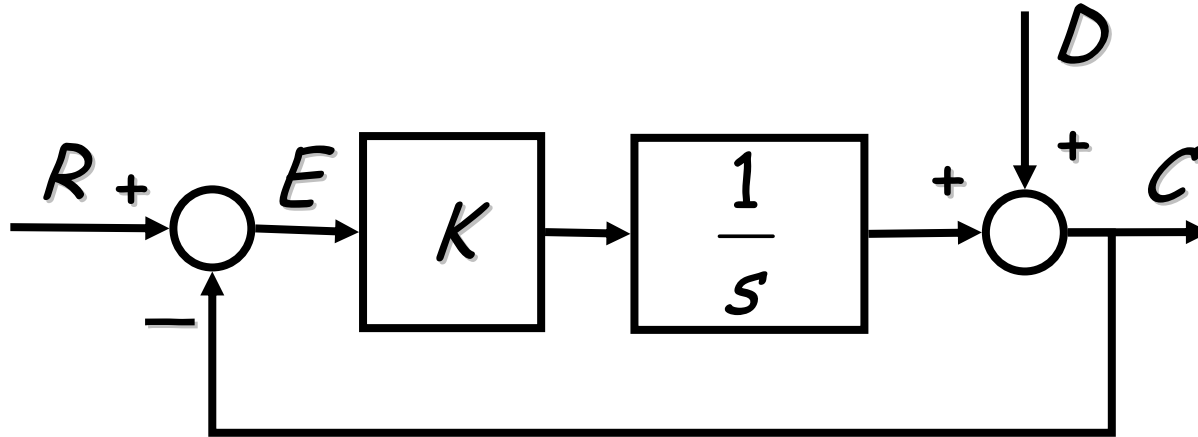
$$\varepsilon_{ss} = \frac{1}{1 + K}$$

20-sim
demo

$$\frac{C}{D} = \left(\frac{1}{1 + K} \right) \left(\frac{s\tau + 1}{s \frac{\tau}{1 + K} + 1} \right)$$



Example (type 1)



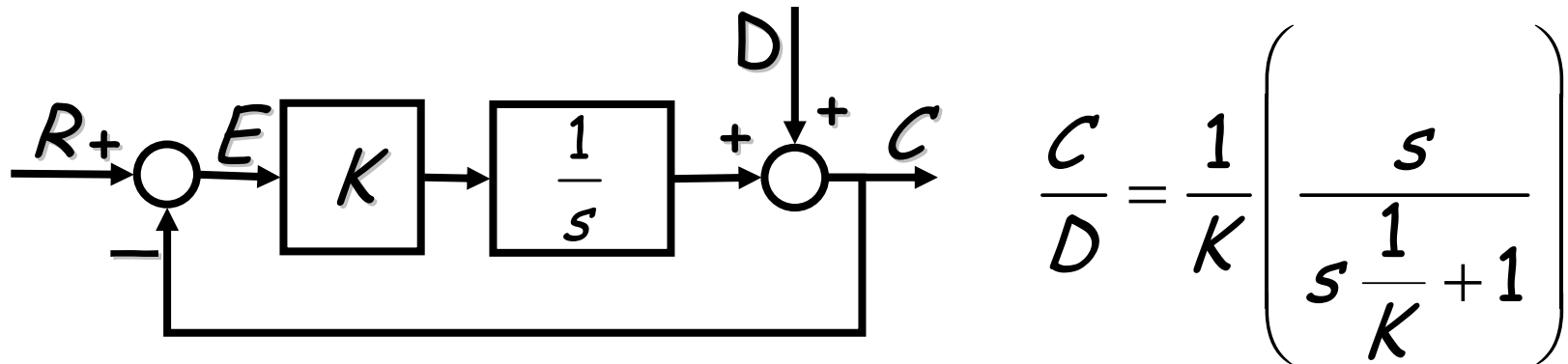
$G(s)$ = first order

of pure
integrators = 1
(type 1)

$$\frac{C}{D} = \frac{1}{1 + \frac{K}{s}} = \frac{1}{1 + KG(s)}$$

$$\frac{C}{D} = \frac{s}{s + K} = \frac{1}{K} \left(\frac{s}{s \frac{1}{K} + 1} \right)$$

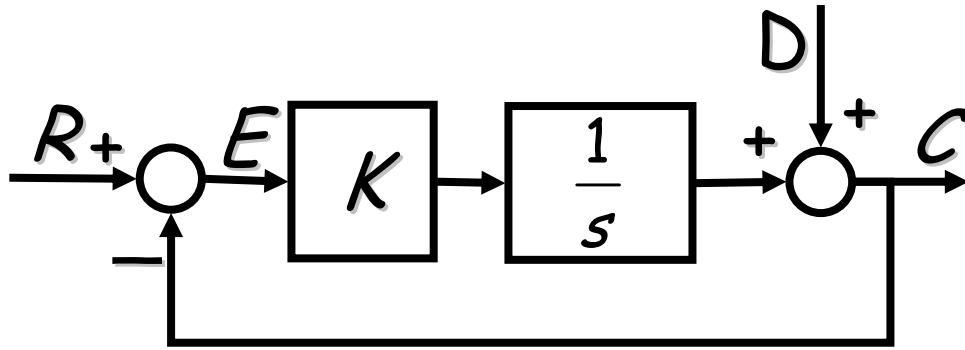
Example (type 1)



if $D = 1/s$

$$\lim_{t \rightarrow \infty} c(t) = \lim_{s \rightarrow 0} \left[\frac{s}{s} \frac{1}{K} \left(\frac{s}{s \frac{1}{K} + 1} \right) \right] = 0$$

Example (type 1)

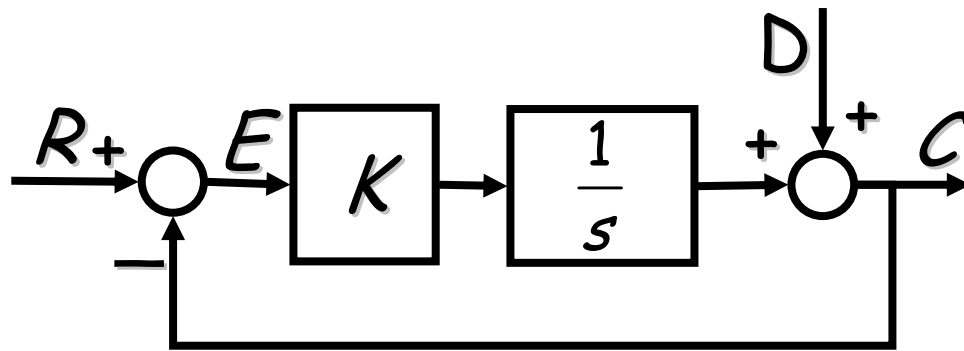


$$\frac{C}{D} = \frac{1}{K} \left(\frac{s}{s \frac{1}{K} + 1} \right)$$

if $D = 1/s$

$$\lim_{t \rightarrow 0} c(t) = \lim_{s \rightarrow \infty} \left[\frac{s}{s} \frac{1}{K} \left(\frac{s}{s \frac{1}{K} + 1} \right) \right] = \frac{1}{K} \frac{1}{\frac{1}{K}} = 1$$

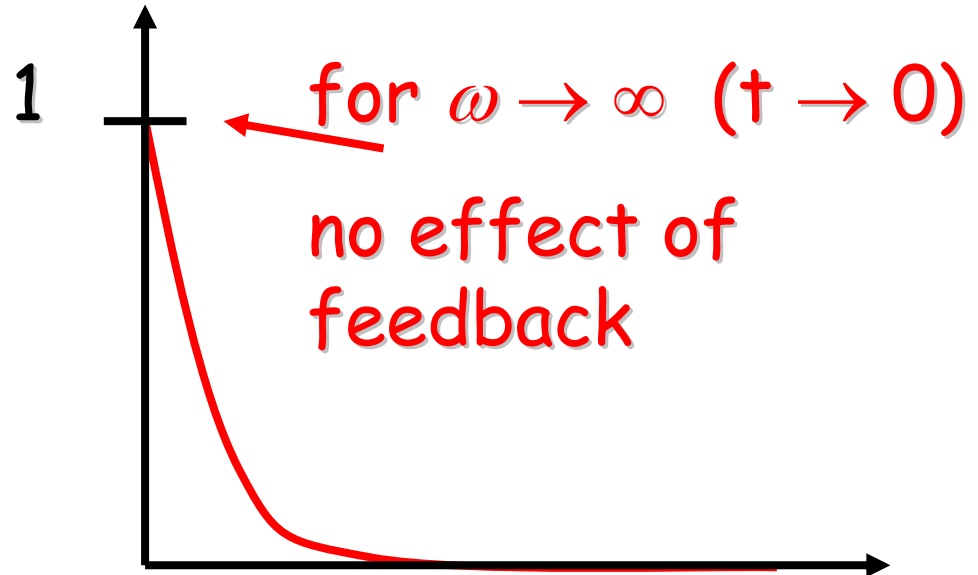
Example (type 1)



$$\frac{C}{D} = \frac{1}{K} \left(\frac{s}{s \frac{1}{K} + 1} \right)$$

steady state
error:

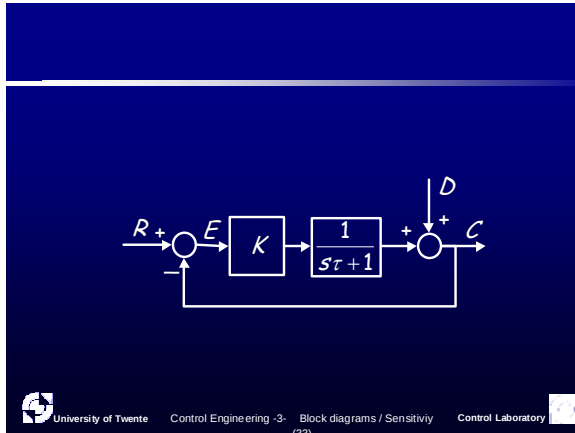
$$\varepsilon_{ss} = 0$$



Steady State Errors

	type 0	type 1	type 2
step: $r(t) = c$	$\frac{1}{1+K}$	0	0
ramp: $r(t) = t$	?		

Ramp (type 0)



$$\frac{C}{D} = \left(\frac{1}{1+K} \right) \left(\frac{s\tau+1}{s \frac{\tau}{1+K} + 1} \right)$$

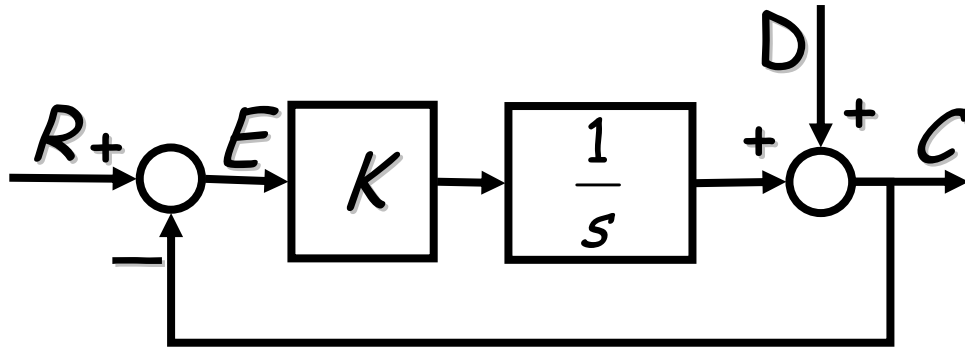
if $D = 1/s^2$

$$\lim_{t \rightarrow \infty} c(t) = \lim_{s \rightarrow 0} \left[\frac{s}{s^2} \left(\frac{1}{1+K} \right) \left(\frac{s\tau+1}{s \frac{\tau}{1+K} + 1} \right) \right] = \lim_{s \rightarrow 0} \frac{1}{s} \rightarrow \infty$$

Steady State Errors

	type 0	type 1	type 2
step: $r(t) = C$	$\frac{1}{1+K}$	0	0
ramp: $r(t) = t$	∞	...	...

Ramp (type 1)



$$\frac{C}{D} = \frac{1}{K} \left(\frac{s}{s \frac{1}{K} + 1} \right)$$

if $D = 1/s^2$

$$\lim_{t \rightarrow \infty} c(t) = \lim_{s \rightarrow 0} \left[\frac{s}{s^2} \frac{1}{K} \left(\frac{s}{s \frac{1}{K} + 1} \right) \right] = \frac{1}{K}$$

Steady State Errors

	type 0	type 1	type 2
step: $r(t) = c$	$\frac{1}{1+K}$	0	0
ramp: $r(t) = t$	∞	$\frac{1}{K}$	0
$r(t) = t^2$	∞	∞	$\frac{1}{K}$

- Determine the steady state errors of the last row of the previous slide
- Simulate type zero and type one systems with step inputs and ramp inputs